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# Determination of Performance of Models In Early Flow Period of A Horizontal Oil Well Using Wellbore Radius As Determinant

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### ABSTRACT

There are some other two-phase IPR methods available in the literature that can be used to predict the performance of oil wells. Hence, in this study, the objective is to carry out a comparison using a wellbore radius as a determinant. The aim is to know how wellbore affects productivity and also to know which model is more reliable in predicting the future performance of a horizontal well. In this work, the IPR curve was developed and used to analyse wells deliverability by estimating the production rate for a given bottom-hole flowing pressure and wellbore radius were used as a determinant. The results show that Wiggin's method has a higher performance. The results have exposed the inflow performance relationship (IPR) of a horizontal oil well at the early flow time. It was observed also that wellbore radius affects productivity and from this, we can convincingly say that Wiggin's method is better in predicting the future performance of a horizontal well.

Keywords: Inflow, Performance, Deliverability, Determinant, Bottom-hole

# **INTRODUCTION**

In the petroleum industry, a horizontal well is a relatively new technology in the oil and gas field development when compared with other methods; (Hawkings et al. 1990; Zhang et al. 2017: Kumar et al. 2018: Li et al. 2018: Ogbamikhumi and Adewole, 2020). Its main advantage is the high productivity per well (Joshi, 2003). The evaluation of the deliverability of the reservoir in the production engineering section is very important. With this, the Inflow Performance Relationship of a well is a connection between its producing bottom-hole pressures and its equivalent production rates under a certain reservoir situation. This shows the producing features of a well. Its results are used in defining the economics of producing a well. The flow of a liquid into a well can be determined by both characteristics of the reservoir and the sand face flowing pressure. By this relationship, a graph is plotted, the bottom-hole flowing pressure on the X-axis, and the production rates on the Yaxis. This is termed the inflow performance relationship curve or IPR curve (Vogel, 1968; Sajedian et al. 2012).

IPR curves are the curves that replicate the ability of the reservoir to deliver fluid to the wellbore. Therefore, IPR curves are important information to analyse the deliverability of wells. Well IPR curves can be built using reservoir parameters. These parameters define the factors (e.g., Productivity index) in the IPR model. The test points (production rate and flowing bottom-hole pressure) are commonly used for generating IPR curves (Al-Jawad et al. 2006).

For single-phase flow, the production rate into a well is directly proportional to the difference between bottom-hole flowing pressure and reservoir pressure, which is called drawdown. IPR curves for single-phase flow result in straight lines with a slope of one over a productivity index or PI. The productivity index is the extent of the gradient of the IPR curve (Tongwen et al. 2019).

Although the horizontal well is a relatively new technology, it is more advantageous as compared to vertical wells. The horizontal well has increased productivity per wells, can access unconventional resources, reduced numbers of well, and thus reducing operational cost (Furui, et al. 2003; Abdullah et al. 2015). The IPR is a correlation between the well bottom-hole flowing pressures and its equivalent flow rates. This indicates the producing characteristics of the well and is used to determine the reservoir deliverability. There

has been various experimental correlations recommended predicting oil well performance under two-phase flow conditions. Some of the key methods are stated below and the first two techniques (Vogel's and Wiggins') will be a focus on in this field. These methods are (Ahmed Tarek, 2006);

(I) Vogel's method

(ii) Wiggins' method

(iii) Standing's method

(iv) Fetkovich's method

(v) The Kleins-Clark method.

Vogel was the first to present an easy-touse technique for predicting the performance of oil wells. His experimental inflow performance relationship (IPR) is founded on computer simulation. There are some other two-phase IPR methods available in the literature and their method that can be used to predict the performance of oil wells.

Hence, in this study, the objective is to carry out a comparison using a wellbore radius as a determinant. The aim is to know how wellbore affects productivity and know which model is more reliable in predicting the future performance of a horizontal well.

# MATERIALS AND METHODS Vogel's inflow performance relationship

To use this relationship, the following steps are taken: Determination of (i) oil production rate (ii) flowing bottom hole pressure (iii) maximum oil production rate and (iv) production rates for other flowing bottom hole pressures at the current average reservoir pressure and data from previous work was used (Oloro, 2014).

$$\frac{Q_o}{(Q_o)max} = 1 - 0.2 \quad \left(\frac{P_{wf}}{P_r}\right) - 0.8 \left(\frac{P_{wf}}{P_r}\right) \quad (1)$$

 $Q_0 = oil flow rate at P_{wf}$ 

 $(Q_o)_{max}$  = maximum oil flow rate at zero wellbore pressure, i.e., AOF

 $P_r$ = present average reservoir pressure, psig  $P_{wf}$ = wellbore pressure, psig

Future flow rate

$$(Q_{omax})f = (Q_{omax})p\left(\frac{(P_{r})f}{(P_{r})p}\right)\left(0.2 + 0.8\left(\frac{(P_{r})f}{(P_{r})p}\right)\right)$$
(2)

NOTE: In this study, the above method is used

for saturated oil reservoir  $P_r \leq P_b$ 

### Wiggins' inflow performance relationship

Wiggins' extended his application to predict future performance by providing expressions for estimating future maximum flow rates. Wiggins' recommended expressions are comparable to that of Vogel's and are expressed as (Wiggins, 1994):

$$\frac{Q_o}{(Q_o)max} = 1 - 0.52 \left(\frac{(P_{wf})}{(P_r)} - 0/48 \left(\frac{(P_{wf})}{(P_r)}\right)^2 \right)$$
(3)

$$\frac{(Q_{omax})f}{(Q_{omax})p} = 0.15 \frac{(P_r)f}{(P_r)p} + 0.84 \qquad \left(\frac{(P_w)f}{(P_r)p}\right)^2 \tag{4}$$

 $(P_r)_r =$  future average pressure  $(P_r)_p =$  current (present) average pressure  $(Q_{omax})_p =$  current maximum oil flow rate  $(Q_{omax})_r =$  future maximum oil flow rate

#### **RESULTS AND DISCUSSION**

The results from this work were obtained by solving for several ? P, which is the drawdown pressure, represented by:

(Pi-Pwf), Wellbore radius (rw), and flow rate (q) keeping the skin (s) constant and also  $_{using}$  J approach, Vogel's, and Wiggins' methods to obtain the IPR curve. The IPR expected is produced by calculating ( $P_i$ - $P_{wf}$ ) for different flow rates used.

Table 1 is showing the values of wellbore radius, x in Ei(-x), and Ei(-x).

As the wellbore radius increases the value of x in EI (-x) increases.

Table 1: Values for Wellbore radius, (rw), x in Ei(-x), and Ei (-x) (Oloro, 2014)

Wellbore radius (r <sub>w</sub>	Values of x in Ei (-x)	Value of Ei (-x)
2.5	0.0444	2.550
2.875	0.0587	2.320
3.125	0.06943	2.160
4.5	0.143	1.521

Given  $\mu$ =0.6cp B<sub>o</sub>=1.2RB/STB, H=100ft  $\phi$ =0.25 K=0.1 S=0 C<sub>t</sub>=1. 5x 10<sup>-5</sup>psi<sup>-1</sup>. For  $r_w$ =2.5in, t

An Official Publication of Enugu State University of Science & Technology ISSN: (Print) 2315-9650 ISSN: (Online) 2502-0524 This work is licenced to the publisher under the Creative Commons Attribution 4.0 International License. 45 Table 2 is representing the values of flow rate, drawdown, and bottom-hole pressure when  $r_w=2.5$  in.

From the table, as the flow rate increase, the bottom-hole pressure decreases while the initial pressure increases with wellbore radius of 2.5 in.

Table 2: Values of Flowrates, Drawdown,and Bottom-hole flowing pressure

Q(STB/day)	P <sub>i</sub> - P <sub>wfr</sub>	$\mathbf{P}_{wf}$
50	161.976	2037.973
100	324.054	1875.95
200	648.108	1551.89
300	972	1228
400	1296	904
600	1944	256

Stabilized flow rate and wellbore pressure = 190STB/day and 1650psig

(Q<sub>o</sub>)<sub>max</sub>=475STB/day and 558.8STB/day for Vogel's and Wiggins' method respectively





Fig. 2 Graph of (Pwf) against (Qo)f at rw=2.5

At the wellbore radius  $(r_w)$  of, 2.5in, the Absolute open flow potential (AOFP) at

 $P_{wf}$ =0psig for Wiggins' method is higher than that of the Vogel's method. The increment started at  $P_{wf}$ =1227. 838psig as shown in figure 1. For the future flow rate, the absolute open flowing potential (AOFP) at  $P_{wf}$ =0psig for Wiggins' method is higher than that of the Vogel's method. The increment started at  $P_{wf}$ =1100psig as shown in figure 2.

Given Bo=1.2RB/STB, H=100ft  $\phi$ =0.25 K=0.1 S=0 C<sub>t</sub>=1.5x 10<sup>-5</sup>psi<sup>-1</sup>  $\mu$ =0.6cp For r<sub>w</sub>=2.875

Table 3 is representing the values of flow rate, drawdown, and bottom-hole pressure when  $r_w=2$ . 875in.From the table, as the flow rate increase, the bottom-hole pressure decreases while the initial pressure increases with a wellbore radius of 2.875 in.

TABLE 3: shows varying values of Flowrates, Drawdown and Bottom-hole flowingpressure

Q (STB/day)	P <sub>i</sub> -P <sub>wfr</sub>	P <sub>wf</sub>
50	147.413	2052.587
100	294.826	1905.174
200	589.651	1610.349
300	884.477	1315.523
400	1179.302	1020.698
600	1768.954	431.046

Stabilized flow rate and wellbore pressure=180STB/day and 1700psig

 $(Q_{o})_{max} = 489.438STB/day$  and 577.718.8STB/day for Vogel's and Wiggins' method respectively



Fig. 3 Graph of (Pwf) against (Qo) at rw=2.875in

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Fig. 4 Graph of (Pwf) against (Qo)f at rw=2.875in

At wellbore radius  $(r_w)$  of 2.875, the Absolute open flow potential (AOFP) at  $P_{uv} = 0$ psig for Wiggins' method is higher than that of Vogel's method as shown in the figure. The increment started at  $P_{wf}$ =1610. 349psig as shown in figure 3. For the future flowrate, the absolute oil flowing potential (AOFP) at P<sub>wr</sub>=0psig for Wiggins' method is higher than that of Vogel's method as shown in figure 4. The increment started at P<sub>wt</sub>=1300psig.

Taken Bo=1.2RB/STB, H=100ft  $\phi$ =0.25  $C_{t}=1.5 \times 10^{-5} \text{psi}^{-1}$  µ=0.6cp for K=0.1 S=0 r\_=3.125in

Table 4 is representing the values of flow rate, drawdown, and bottom-hole pressure when r\_=3.125 in.

From the table, as the flow rate increase, the bottom-hole pressure decreases while the initial pressure increases with a wellbore radius of 3.125 in.

Table 4: shows varying values of Flowrates, Drawdown, and Bottom-hole flowing pressure

Q(STB/day)	P <sub>i</sub> - P <sub>wfr</sub>	$\mathbf{P}_{wf}$
50	137.246	2062.754
100	274.493	1925.507
200	548.986	1651.014
300	823.478	1376.522
400	1097.971	1102.029
600	1646.957	553.043

Stabilized flow rate and wellbore pressure = 175STB/day and 1750psig

 $(Q_{\rm o})_{\rm max}{=}522.840 STB/day$  and 619.153 STB/dayfor Vogel's and Wiggins' method respectively





At wellbore radius  $(r_w)$  of 3. 125in, the Absolute open flow potential (AOFP) at P<sub>wf</sub>=0psig for Wiggins' method is higher than that of the Vogel's method. The increment started at  $P_{wf}$ =1376. 522 psig as shown in figure 5. For the future flow rate, the absolute oil flowing potential (AOFP) at P<sub>wt</sub>=0psig for Wiggins' method is higher than that of the Vogel's method. The increment started at P<sub>wf</sub>=1300psig as shown in figure 6.

Take B<sub>o</sub>=1.2RB/STB, H=100ft  $\phi$ =0.25 K=0.1 S=0 C<sub>1</sub>=1.5x  $10^{-5}$  psi<sup>-1</sup>  $\mu$ =0.6cups of raw=4.5 Table 5 is representing the values of flow rate, drawdown, and bottom-hole pressure when r\_=4.5in.

From the table, as the flow rate increase, the bottom-hole pressure decreases while the initial pressure increases with a wellbore radius of 4.5 in.

Table 5: shows varying values of Flowrates, Drawdown, and Bottom-hole flowing pressure for r<sub>w</sub>=4.5in

Q (STB/day)	Pi- Pwfr	Pwf
50	96.644	2103.356
100	196.289	2006.711
200	386.577	1813.423
300	579.8 66	1620.134
400	773.155	1426.845
600	1159.732	1040.268

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Stabilized flow rate and wellbore pressure=170STB/day and 1800psig (Q<sub>o</sub>)<sub>max</sub>=565.109STB/day and 671.344STB/day for Vogel's and Wiggins' method respectively



Fig. 7 Graph of (Pwf) against (Qo)f at rw=4.5



At the wellbore radius ( $r_w$ ) of 4.5, the Absolute open flow potential (AOFP) at  $P_{wf}$ =0psig. The increment started at  $P_{wf}$ =1620. 134psig as indicated in figure 7. For the future flow rate, the absolute oil flowing potential (AOFP) at  $P_{wf}$ =0psig for Wiggins' method is higher than that of the Vogel's method. The increment started at  $P_{wf}$ =1800psig as shown in figure 8.

Inflow Performance Relationship (IPR) defines the performance of flow rate with flowing pressure, which is a significant tool in understanding the well productivity. Two models were used in this study and the results were presented as shown above. To validate this work, Ahmed, et al (2017) work was used. Their work shows that the Wiggins method is more reliable in predicting the future performance of a horizontal well.

#### CONCLUSION

Finally, it can be seen that the studies have exposed the inflow performance relationship of a horizontal well at the early flow time. We can see that the effect of the wellbore radius on productivity. When there is an increase in wellbore radius, there was an additional pressure drop. Also, we can convincingly say that Wiggins' method is better than Vogel's method. The future flow rate was also determined using both Wiggins' method and Vogel's method, and Wiggins' method is better than Vogel's method.

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### REFERENCES

- Abdullah Al Q, Hasan AlH, Hasan AlY. (2015). A New Approach for Optimization of Long Horizontal Wells' Performances, International Petroleum Technology Conference, 6-9 December, Doha, Qatar. pp:60-61.
- Ahmed T. (2006). Reservoir Engineering Handbook, Elsevire Inc. (3<sup>rd</sup>ed), ISBN 13: 978-0-7506-7972-5-334-336.
- Ahmed MD, Mahmoud AS, Abdel AH, Sayyouh MH. (2017). Inflow Performance Relationship Correlation for Solution Gas-Drive Reservoirs Using Non-Parametric Regression Technique. The Open Petroleum Engineering Journal (TOPEJ). 10;(1):152-176.
- Batruna M, Daggez A. (2010). Drilling and Completion of Horizontal wells Al– Fatah University Press, Tripoli, Libya. 1<sup>st</sup> Edition. pp:1-22.
- Al-Jawad MS, Ottba DJS. (2006). Well Performance Analysis Based on Flow Calculations and IPR, Journal of Engineering. 13;(3): 822-841.
- Hawkings N, Ramsey C, Rapach J, Kristof M. (1990). Results from a Horizontal Well, in a Rotliegendes Gas Field, Society of Petroleum Engineers, European Petroleum Conference. 21 -24 October, The Hague, Netherlands, pp: 441.
- Kumar M, Sharma P, Gupta DK. (2018). Sensitivity study of horizontal length, offset from water-oil contact, and withdrawal rate of horizontal well in bottom water drive Reservoir. J Petrol Explor Prod

Technol. 8:577-588.

- Li Q, Xiao J, Zeng Q. (2018). Performance of Horizontal Wells with Inflow Control Devices in Homogeneous Reservoirs with Bottom Water Drive. Arab J Sci Eng. 43:2473–2479.
- Ogbamikhumi AV, Adewole ES. (2020). Pressure Behavior of A Horizontal Well Sandwiched Between Two Parallel Sealing Faults, Pressure Behavior of a Horizontal Well Sandwiched Between Two Parallel Sealing Faults. Nigerian Journal of Technology. 39(1):148-153.
- Oloro J. (2014). Comparison of inflow Performance Relationship in Vertical Well using Constant J and Vogel's Method. African Journal of Physics. 7:113-123.
- Sajedian A, Ebrahimi M, Jamialahmadi M. (2012). Twophase Inflow Performance Relationship Prediction Using Two Artificial Intelligence Techniques:

- Multi-layer Perception Versus Genetic Programming. Petroleum Science and Technology. 30;(16):1725-1736.
- Vogel JV. (1968). Inflow Performance Relationships for Solution-Gas Drive Wells, Journal of Petroleum Technology. 20(1):83-92.
- Wiggins M. (1994). Generalized Inflow Performance Relationships for Three-Phase Flow. SPE Res Eng 9(3):181-182.
- Tongwen J, Hedong S, Xingliang D. (2019). Carbonate gas reservoirs, Dynamic Description The technology of Fractured Vuggy Carbonate Gas Reservoirs, Elsevier In, 1st Edition, ISBN 978-0-12-818324-3:233-307.
- Zhang W, Jiang R, Xu J, Gao Y, Yang Y. (2017). Production performance analysis for Horizontal wells in composite coal bed methane reservoir. Energy Exploration and Exploitation. 35 (2):194–217.